

A 9-10.6 GHz MICROSTRIP ANTENNA - UWB LOW NOISE AMPLIFIER WITH DIFFERENTIAL NOISE CANCELING TECHNIQUE FOR IOT APPLICATIONS

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Abstract. An ultra wide band (UWB) receiver front-end operates at the UWB frequency range, starting from 9 GHz-10.6 GHz is proposed in this paper. The proposed system consists of an off-chip microstrip antenna and CMOS differential low noise amplifier with a differential noise canceling (DNC) technique. The proposed antenna is trapezoidal dipole shaped with balun and printed on a low-cost FR4 substrate with dimensions $10 \times 10 \times 0.8$ mm³. The balun circuit integrated with the ground antenna to improve the antenna impedance matching. Full-wave EM solver HFSS (High Frequency Structure Simulator) is used for modeling the proposed antenna. The CMOS LNA is designed using UMC 0.13 μ m CMOS process, and exhibits a flat gain of 19dB, maximum noise figure of 2.9 dB, 1dB compression point -16dBm, 3rd order intercept point (IIP3) -10dBm, and DC power consumption of 2.8 mW at 1.2 V power supply. Applying the noise canceling stage, the NF is reduced by 50% to be 2.75 dB while the power consumption is increased to be 2.9mW.

Keywords: ultra-wideband (UWB), low noise amplifier (LNA), differential noise canceling, low power, low noise figure.

1. Introduction

Recently, rapidly progress are made in ultra-wideband (UWB) applications with high data rate communications in short distances with low fabrication cost as internet of things (IoT) [1]. IoT connects billions of objects to form a huge network for communications and perform smart actions. There aren't any standard definitions for IoT

[2]. Various definitions are listed as IoT allows things and people to be connected anywhere, and are widely used for sensing applications, security purposes and high data rate 5G communications since it enables robust wireless systems in dense multipath scenarios [3]. In this paper, a complete UWB receiver for IoT applications is proposed. Wide band has ability for deep wall penetration as well as resolution of sub-nanosecond delays in centimeter-level distance resolutions. Added to this is an improvement on the timing resolution compared to conventional narrowband signals. In addition to broadband gain and input matching requirements, the broadband standard also poses a tight specification on the band switching time, thus precluding the direct synthesis of frequencies by phase locking. An approach suggested for this task incorporates a single phase-locked loop (PLL) and wideband mixer to generate different frequencies that are present at all times and could simply selected as the local oscillator (LO) signal [4]. Compact low-power consumption antennas that can be easily embedded within the system are considered essential for portable IoT devices [5].

UWB antennas used planar microwave circuitry have generated attractive radiating structures with high gain, low weight, reliability, ease of manufacturing and integration such as the Vivaldi antennas and the tapered slot antenna. UWB has many definitions as IEEE (the operating bandwidth greater than 20% antennas [1]) or as FCC (released in 2002 that the UWB protocol that covers the frequency ranges from 3.1-10.6 GHz). UWB planar microwave circuitry have generated attractive radiating structures with high gain, low weight, reliability, ease of manufacturing and integration such as the Vivaldi antennas [6-7], and the tapered slot antenna [8-9] and planar log-periodic dipole (LPDA) [10-11].

In this paper a complete wideband receiver- front end operates in the frequency range 9-10.6 GHz is proposed. Fig.1 shows the block diagram for the proposed receiver, which consists of the off-chip microstrip antenna, a balun and on-chip CMOS low noise amplifier (LNA). The LNA is implemented using UMC 130 nm CMOS technology with a simple noise canceling technique.

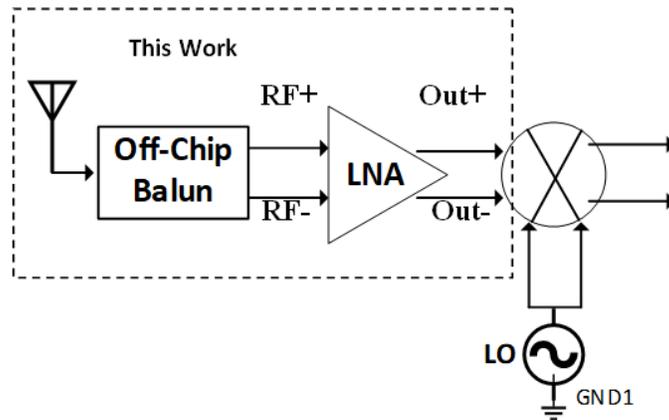


Fig. 1 Block diagram of the propose UWB receiver.

The paper is organized as follows; section II describes the design and analysis of the proposed broadband antenna in terms of reflection coefficient, antenna impedance, efficiency and antenna gain. Ssection III introduced the UWB low noise amplifier with differential noise canceling (DNC) technique. While section IV shows the system simulation, finally, section VI concludes the proposed work.

2. Wideband Antenna Design

In this section a new proposed wide bandwidth antenna is presented which consists of a combined structure of different lengths of printed trapezoidal dipole fed by CPW and balun circuit to improve the impedance matching. The proposed antenna as shown in Fig. 2 has been designed with 3D electromagnetic simulation HFSS ver. 14. The proposed antenna dimensions are $10 \times 10 \times 0.8 \text{ mm}^3$ when printed on a FR4 dielectric substrate. The proposed CPW trapezoidal dipole antenna introduces UWB with the multiple resonant properties. Fig.2 shows the geometry and dimensions of the proposed antenna and the final dimensions are shown in table 1. To improve the antenna bandwidth modified rectangular dipole is used by using two different bases width and etching balun to improve the impedance matching with suitable dimensions is used as shown in Fig.3. These wideband are used for different wireless communications applications and for UWB applications. The antenna is fed by $50\text{-}\Omega$ transmission line (TL), which can be easily integrated with other microwave circuits printed on the same substrate.

The proposed antenna is fabricated by using photolithographic technique and it is measured by using a Rohde & Schwarz ZVA67 vector network analyzer (50MHz to 67GHz). Then the comparison results between simulated and measured of the proposed antenna for both reflection coefficient and antenna impedance real and imaginary are shown in Fig. 3(a). This figure shows that good agreement between measured and simulated results and 50Ω input impedance with zero imaginary part of the proposed antenna at 7.8 GHz with reflection coefficient $|S_{11}|=-37\text{dB}$ with wideband extend from 7 GHz to 12 GHz at -6dB reflection coefficient which is wide enough to cover the FCC approved UWB in addition to wireless communications. Fig. 3(b) shows that the antenna gain and radiation efficiency for the proposed antenna. It is very clear that the antenna has suitable gain in the frequency range of operations about 3.5 dBi in average while the antenna radiation efficiency has about 80%.

Table 1. Dimensions of the proposed antenna (dimensions in mm).

W_{sub}	L_{sub}	W_g	L_g	g	S
10	10	4.8	2.8	0.2	1.8
W_f	d	L_s	L_f	W_1	W_2
0.77	0.9	1.75	4.9	2	4.375

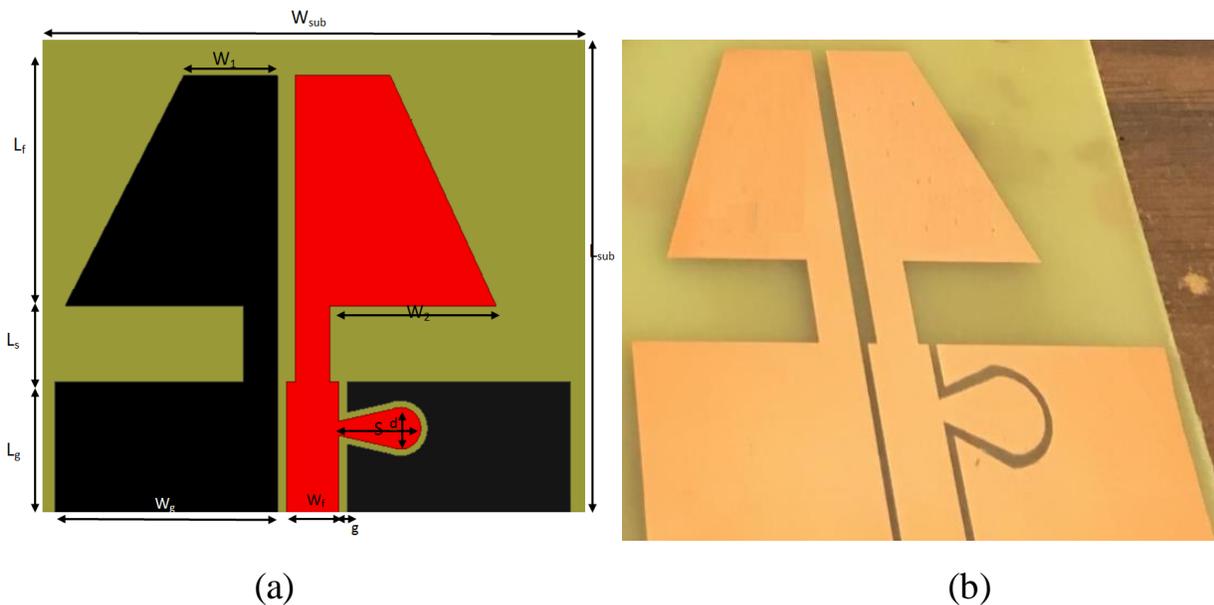


Fig.2: (a) Layout of the proposed trapezoidal dipole antenna and (b) photo of the fabricated antenna.

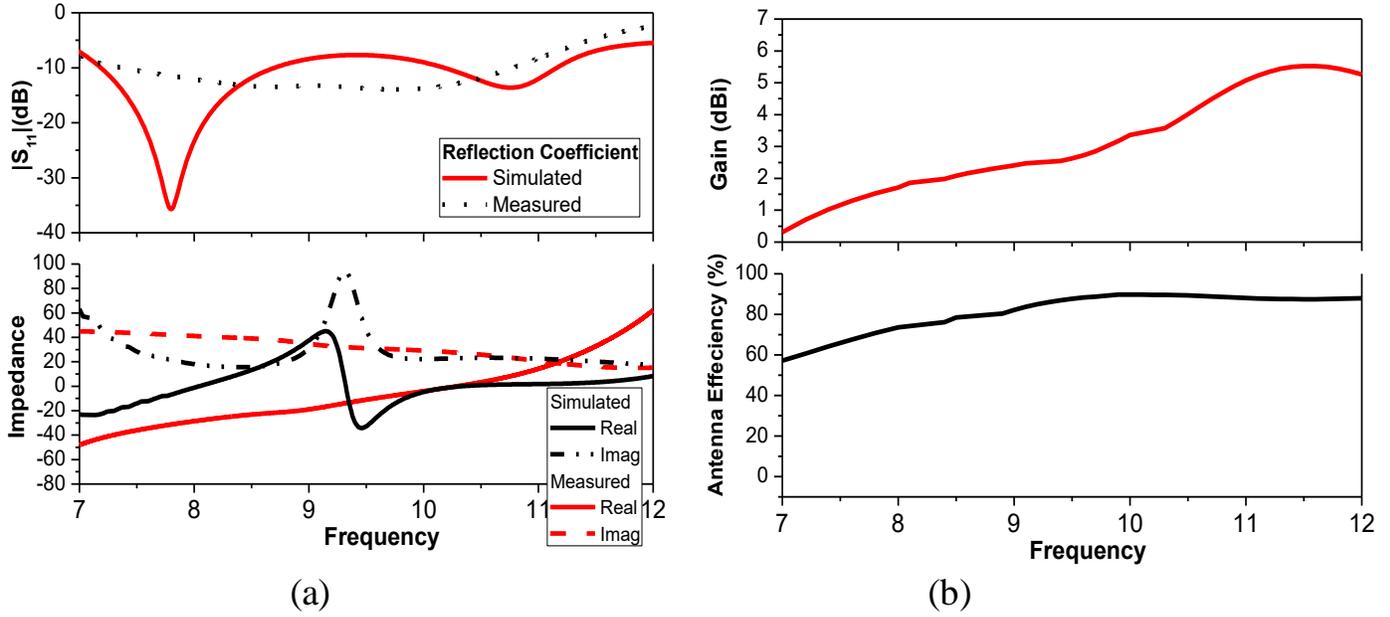


Fig. 3: (a) Simulated and measured results of the proposed antenna $|S_{11}|$ with the impedance (real and imaginary) and (b) Simulated gain and radiation efficiency of proposed dipole.

3. UWB Low Noise Amplifier with Differential Noise Canceling (DNC)

Technique

Fig. 4(a) shows a previously reported noise canceling technique [12-15] depends on creating two signals - with two different gain and phase - using 2 amplifiers A_x and A_y , the 2 generated signals are subtracted such that the noise is canceled. Fig. 4(b) shows our proposed technique, for a 2-stage differential amplifier with two branches each has a gain $A_1 A_2$. Each branch uses only one noise canceling amplifier A_{nc} , the output of the noise-canceling amplifier in each branch is added to the input of amplifier A_2 of other branch, which can be considered as subtraction technique. Fig. 5(a) shows circuit diagram for the proposed LNA. It consists of two-stages, a cascade common source common gate (CS-CG) amplifier – M_1 to M_4 - with inductive load L_1, L_2 and a shunt feedback common source (SF-CS) amplifier – M_5 and M_6 - to obtain the wideband frequency of operation with an inductive output load L_5, L_6 [12]. Inductive interstage network – L_3, C_1 and L_4, C_2 - is set between the two stages to improve gain bandwidth performance [16].

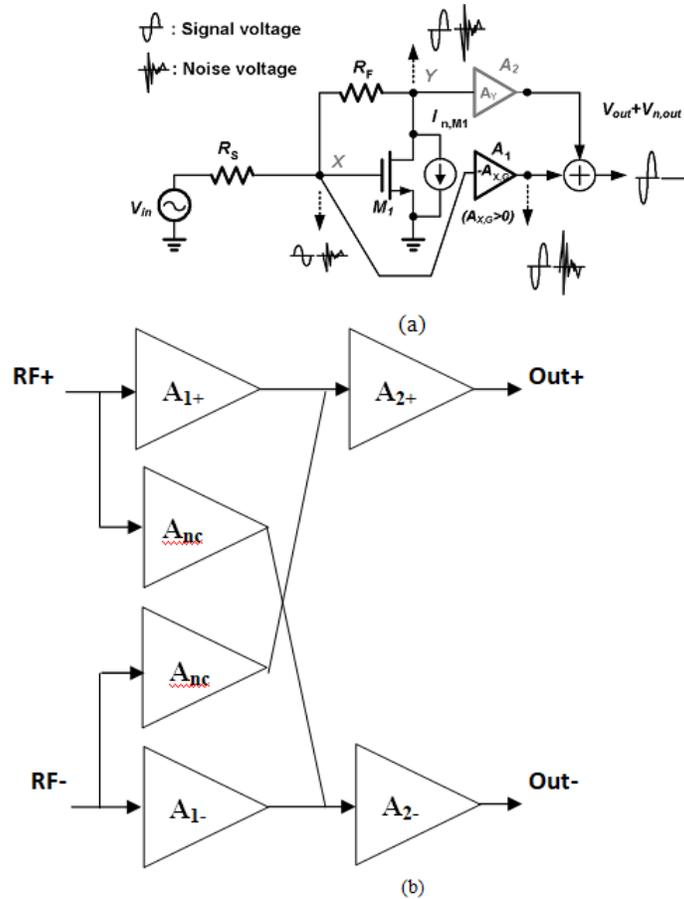


Fig. 4. (a) Previously reported gain-enhanced noise-canceling technique [16] and (b) Proposed differential noise canceling technique.

M_7 and M_8 represent the noise canceling amplifiers with their biasing resistances R_b . Simulation for the LNA connected to a 50Ω load terminal with and without noise canceling blocks is shown in Fig.6. Fig.6(a) shows a flat gain with maximum 19dB and 0.5 dB gain attenuation between maximum and minimum gain in the frequency band 9-10.6 GHz, while Gain NC represents the gain with the noise canceling blocks that improves the flatness of the gain and widens its bandwidth. Fig.6(b) shows that the LNA has 5.5dB NF at 10GHz, adding the noise canceling blocks reduces NF to 2.75dB which is considered a good improvement compared with other low noise topologies that uses inductors with large area compared with the blocks added. The proposed LNA has a DC power dissipation 2.8/2.9mW

M ₁ -M ₄ (μm)	M ₅ -M ₆ (μm)	M ₇ -M ₈ (μm)	L ₁ , L ₂ (nH)	L ₃ , L ₄ (nH)	L ₅ , L ₆ (nH)	C ₁ , C ₂ (pF)	C _{nc} (pF)	R _{FB} (Ω)	R _{nc} (Ω)	R _b (Ω)
224/0.13	115.2/0.3	28.8	1	2.3	3	0.3	0.9	200	100	12K

4. System Simulation

The complete receiver front-end—including antenna S-parameters - is simulated to check the complete system performance. Fig.7 (a) shows flat gain in the band of operation 9-10.6GHz with slight variation compared with LNA gain (Gain NC) shown in Fig 6(a) which shows the perfect matching between the balun and LNA. Fig.7 (b) shows that maximum Noise Figure NF is 3dB in the band of operation. The linearity is shown in Fig.7(c) with 1dB compression point -16dBm, 3rd order intercept point (IIP3) -10dBm. Fig.7(d) shows a good matching between antenna and LNA with input reflection coefficient <-10dB. Table 3 shows a comparison between the proposed system and other UWB receivers' front –end.

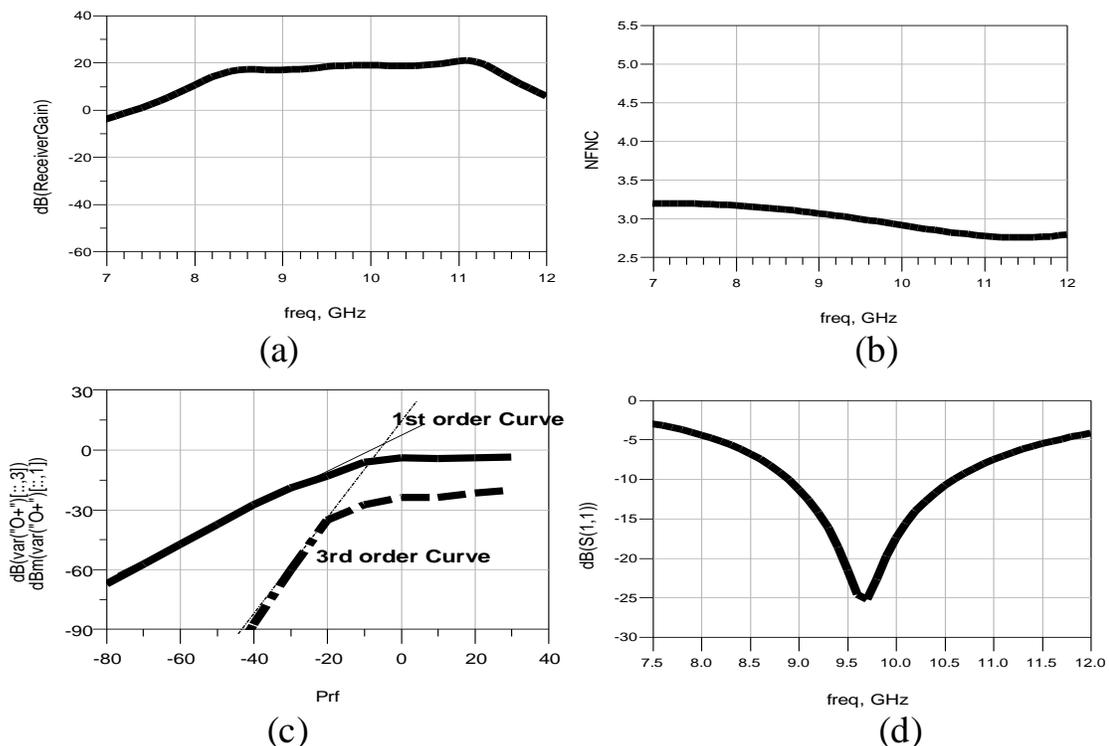


Fig. 7 Complete receiver front-end simulation Performance (a) gain (b) Noise Figure, (c) linearity and (d) input matching.

It is clear from the table that the proposed system has very low power dissipation, high gain and low NF compared with other topologies. Although, the IIP3 is low but it could accept for UWB receivers. Moreover, the proposed LNA has limited number of on-chip inductors, which lead to small implementation area. All these specifications make it suitable for low power applications as IoT, WSN and general sensing applications.

Table 3. Performance Comparison with previously reported UWB LNA

Ref.	[16]	[17]	[18]	[19]	[20]	This work
Technology	0.18 μ m	0.09 μ m	0.18 μ m	0.13 μ m	0.18 μ m	0.13 μ m
Frequency (GHz)	3.2 -6.3	2.4 - 10.4	3.1 -4.9	3-12	3 -10	9 -10.6
Gain (dB)	15	9.5	14.1	13.5	13.7	19
IIP3 (dBm)	N/A	13.1	-6.7	-7	-0.2	-10
Noise Figure (dB)	0.95	4	4.29	4.3	2.2	2.9
Supply (V)	1.8	1.2	1.8	1.2	1.8	1.2
Power Dissipation(mW)	4.7	14.8	4.5	8.5	18	2.9

V. Conclusion

This paper has proposed a low power, low NF UWB receiver front-end. The proposed system consists of an ultra-wideband CPW-fed trapezoidal dipole shaped antenna and a CMOS LNA. The dipole antenna creates an ultra-wideband extended from 7 GHz to 12 GHz. The LNA consists of two stages with Inductive interstage network to increase BW and a noise canceling stage to improve NF with simple MOSFET. The proposed system has a 19dB flat gain in the frequency band 9-10.6 GHz with low NF 2.75dB, low DC power consumption 2.9mW which make it suitable for IoT technology and sensing applications.

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