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### ANALYSIS OF THE PROPAGATION, TRANSFORMATION AND SCATTERING OF THE MONOCHROMATIC ELECTROMAGNETIC WAVES IN THE IRREGULAR WAVEGUIDES: A CASE OF INTEGRATED-OPTICAL WAVEGUIDE WITH STATISTIC SURFACE ROUGHNESS AND A CASE OF OPTICAL NANOFIBERS WITH RANDOM ROUGH SURFACE

A.A. Egorov,<sup>1</sup> A.V. Stavtsev,<sup>2</sup> T.K. Chekhlova,<sup>2</sup> A.G. Timakin,<sup>2</sup> V.I. Grygoruk,<sup>3</sup> Yu.A. Gayday,<sup>3</sup> A.V. Kovalenko,<sup>3</sup> V.N. Kurashov<sup>3</sup>

<sup>1</sup>A.M. Prokhorov General Physics Institute, Russian Academy of Sciences, <sup>2</sup> Peoples' Friendship University of Russia <sup>3</sup> Taras Shevchenko National University of Kyiv

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**Abstract**. We examine in this paper two cases, which are very interested for the theory and experiments: a case of an integrated-optical waveguide with statistic surface roughness and a case of optical nanofibers with random rough surface. The peculiarities of approximate solutions of vector electrodynamic problems in the first cases in brief are discussed and useful evaluations of losses due to scattering also are given. Some results of research of radiation losses of optical nanofibers in assumption of Gaussian statistics of distorted glass/air interface are presented. In conclusion we mark a problem of synthesizing of an optical processor or/and optical sensor with high metrological parameters with allowance for the problem of light scattering in optical waveguides with surface roughness.

**Keywords:** integrated optics, fiber optics, Maxwell's equations, vector electrodynamics' problems, irregular waveguide, multilayer waveguide, optical nanofibers, boundary conditions, waveguide modes, statistic irregularities, TE and TM modes, leaky modes, waveguide scattering, radiation losses, optical sensor, computer modelling.

### 1. Introduction

A lot of papers are devoted to the analysis of propagation of an electromagnetic wave in a planar multilayer regular dielectric two-dimensional (2D) waveguides (see, for example, [1-8]). A number of methods (see for example references [1-13]) are used for an analysis of processes of propagation and transformation of (wave)guiding, quasi-guiding and leaking modes, accompanying an exchange of energy among modes and between modes with surroundings in irregular waveguides.

The integrated-optical waveguide is one of basic elements of the integrated optics and waveguide optoelectronics [2, 4, 6, 7, 9, 10]. In most cases waveguide serves as the basis for creation of the various optical integrated circuits [4]. In this connection the important direction in technology is the development of methods of creation of a waveguide with a low level of losses of the intensity of the directed mode on scattering by three-dimensional (3D) irregularities (boundaries roughness and/or heterogeneities of the waveguide layers; smooth irregularities) of the structure of a waveguide.

In the paper we study two interested cases: a case of an integrated-optical waveguide with statistic surface roughness and a case of optical nanofibers with random rough surface.

The light scattered in a waveguide can be registered [2-10, 12-37]: i) like radiated substrate-cover (substrate-air) radiation modes, and/or substrate radiation modes, or leaky modes, and as the radiation, scattered in the plane of a waveguide in the case of boundaries roughness and/or heterogeneities of the waveguide layers; ii) like diffracted and/or leaky waves in the case of smooth irregularities.

As a rule, when analysing the waveguide scattering one gives main attention to the solution of the direct scattering problem i.e. to the determination of the field's or to the intensity's characteristics of the coherent radiation scattered in the waveguide. The found scattering diagrams (patterns) then can be used for the solution of an inverse problem [28, 33, 34] by the known comparison method, when one tries by that or different way to achieve the coincidence, for example, by the least squares

2

method (in rms sense) of the experimentally measured diagrams with the theoretically calculated one.

When neglecting polarizing effects the problem of waveguide 3D scattering is reduced to a solution of known 2D wave equation. Then we assume absence of the cross-correlation relations between all types of irregularities (roughness of the boundaries and/or heterogeneity of the layers of waveguide).

Progress in fiber optics technologies caused attention to the problem of radiation losses induced with a roughness of a waveguide surface [40]. The open surface of the waveguide core has a structure of frozen capillary wave. As formation of such structure results from equilibrium thermodynamics, it can not be eliminated by means of technology. Therefore, the roughness induced radiation losses are intrinsic in the waveguides with glass/air interface. These losses are considered to be critical when essential part of the light power is carried with an evanescent wave, particularly in photonic crystal waveguides [41, 42], and optical nanofibers [44, 45].

The waveguide scattering method is the most suited tool for the metrological control in the integrated optics since the determined characteristics and parameters of waveguide irregularities characterize the waveguide in a whole just as an integrated structure but not as the separated mediums used for its manufacture [14-22, 24, 25, 28, 33]. The important advantage of the waveguide scattering method is that it allows increasing sensitivity of measurements in ~  $10^2$ - $10^3$  on a comparison with methods of single light scattering, due to repeated in phase scattering of the light on researched statistical irregularities. Other advantage of this method is the possibility of the research of scattering in a broad band of the variation of values of the lateral sizes of irregularities, including the size about the light wavelength [28-34, 39].

### 2. Scattering of electromagnetic monochromatic waves in an integratedoptical waveguide with statistic irregularities. Main equations

The scattering problem of a directed waveguide mode in a planar dielectric waveguide containing stochastic irregularities can be solved with the help of the theory of perturbations [2, 18, 24, 25, 28, 31-34, 39].

Generally for the description of an electromagnetic field  $\mathbf{E}$  in an irregular integrated-optical waveguide (see fig. 1) one can use the following vector equation:

$$\nabla^{2}\mathbf{E} + \nabla \left(\mathbf{E}\frac{\nabla \varepsilon}{\varepsilon}\right) + \omega^{2}\varepsilon\mu\mathbf{E} = 0, \qquad (1)$$

where  $\omega$  is the electromagnetic field frequency;  $\varepsilon = \varepsilon_r \varepsilon_0$ ,  $\mu = \mu_r \mu_0$ ;  $\varepsilon$  and  $\mu$  are the dielectric permittivity, and magnetic susceptibility, respectively;  $\varepsilon_0$  and  $\mu_0$  are the electric and magnetic constants, respectively;  $\nabla$  is the well-known vector differential operator, and  $\nabla^2 = \Delta$  is Laplacian. This equation is fair in the rectangular Cartesian coordinates. The equation (1) is found with the help of the Maxwell's equations.

We consider the case of propagation in a waveguide along z-axis of the main TE-mode (for TM-mode the analysis is carried out similarly). Next we can write equation (1) as the approximate three-dimensional equation [28, 31-34, 39].

Keeping in the obtained equation only members of the first order of smallness in respect of  $\mathbf{E}_s$  and  $\Delta \varepsilon(\mathbf{r})$ , we shall receive an approximate inhomogeneous wave equation, which can be considered as a homogeneous wave equation with perturbation as a source  $\mathbf{E}_{0y}$  in the right part:

$$\nabla^{2}\mathbf{E}_{s}(x, y, z) + \omega^{2}\mu\varepsilon_{0m}\mathbf{E}_{s}(x, y, z) \approx -\omega^{2}\mu\varepsilon_{0m}\Delta\varepsilon_{m}(x, y, z)\mathbf{E}_{0y}(x, z), \qquad (2)$$

where  $\mathbf{E}_{0y}$  is the solution of the homogeneous undisturbed equation circumscribing the propagation of the main TE-mode in a waveguide forming of *m*-layers.



**Fig. 1**. A three-layer (m = 3) irregular integrated-optical waveguide: 1 is the covering layer, 2 is the guiding layer, 3 is the substrate, 4 is the optical ray, 5 is the light scattered on the surface roughness; h is the waveguide thickness. The optical ray 4 is

propagating along the axes *z*, undergoing the infringed total internal reflection on the rough boundaries of the waveguide.

From the power point of view, the "*source*" in a right part of the equation (2) is the intensity of the mode, incident on an irregular area of waveguide and scattered in all enclosing space (3-D *scattering*).

The solution of the given inhomogeneous wave equation can be obtained as a convolution of some Green function G(x, y, z; x', y', z') with the expression for the source  $\Delta \varepsilon(x', y', z')$ :

$$\mathbf{E}_{s}(x, y, z) = -\omega^{2} \mu \varepsilon_{0} \iiint \Delta \varepsilon(x', y', z') G(x, y, z; x', y', z') \mathbf{E}_{0y}(x', z') dx' dy' dz'.$$
(3)

The analysis shows, that in this case it is impossible to neglect polarizing effects and the consideration of the problem of waveguide scattering of light on threedimensional irregularities becomes hardly complicated, since the determination of analytical expression for a Green function represents here not at all trivial problem.

When neglecting the polarizing effects, originating during scattering, it is enough to require, that the relative variation of the dielectric permittivity on a distance of one wavelength was much less than unit. Then it is possible to use a simple wave equation:

$$\Delta \mathbf{E} + n^2 k_0^2 \mathbf{E} = 0, \qquad (4)$$

which is fair for each Cartesian component of the vector of electrical field. For fundamental TE-mode, propagating along the axes z, under condition  $\partial/\partial y = 0$ , the formula (4) accepts next form:

$$\frac{\partial^2 E_y}{\partial x^2} + \frac{\partial^2 E_y}{\partial z^2} + n^2 k_0^2 E_y = 0, \qquad (5)$$

where  $n^2(x,z) = n_0^2(x,z) + \Delta n^2(x,z)$ ,  $n_0^2(x,z)$  describes regular properties of an appropriate medium of waveguide (accepts values  $n_1$ ,  $n_2$  or  $n_3$  accordingly), and the component  $\Delta n^2(x,z)$  describes irregularities of the structure of a waveguide (both irregularity of the boundaries, and heterogeneity of a refraction index).

For application of the theory of perturbations the addendum  $\Delta n^2(x,z)$  should not be necessarily the value of the small order. There is quite enough, that the area, within the limits of which this component differs from zero, was very narrow. The solution of the equation (5) with help of the approximate method of "*ideal modes*" [2] is then finding as the expansion of certain scattering field on the orthogonal set of the modes of the rectilinear optical waveguide.

Thus the solution for component of a scattered field in any point of space with coordinates x, z takes form:

$$E_{y} = \int q(\tilde{\rho}; L) E_{y}(\tilde{\rho}; z) d\tilde{\rho}, \qquad (6)$$

where q is the effective amplitude of scattering TE-modes, defined as factor of expansion of a field on all radiation modes;  $\tilde{\rho}$  is the transversal component of the propagation constant of the radiation modes (see fig. 2).

On the fig. 2 the diagram of the wave numbers  $\beta$  and  $\rho$  are presented:  $\beta^2 + \rho^2 = (kn_m)^2$ ,  $k = 2\pi/\lambda$ , m = 1, 2, 3; **K** is a certain harmonic lattice vector in the infinitive spectrum of the irregularities;  $\theta$  is the scattering angle in the *xz* plane of incidence. Here  $\beta$  represents the longitudinal component of the propagating constant of radiating modes.

The factors of expansion are fined from the orthogonality relations with the help of the theory of perturbations. Both numerical methods of direct calculation and analytical methods of determination of an approximate value of the integral in expression (6) can be used, for example, method of the stationary phase or saddle point method.

If the condition  $\partial/\partial y = 0$  is executed, it is possible to express any distribution of the field of a waveguide as the superposition of orthogonal TE- and TM-modes of an ideal rectilinear waveguide [2]:

$$E_{y} = \sum_{\nu} c_{\nu} E_{\nu y} + \sum_{0}^{\infty} q(\rho) E_{y}(\rho) d\rho,$$

where the first sum is distributed to all guided even and odd TE-modes, and the

combination of the sum and integral takes into account all radiation modes.

Similarly for TM-modes:

$$H_{y} = \sum_{\nu} d_{\nu} H_{\nu y} + \sum_{0}^{\infty} p(\rho) H_{y}(\rho) d\rho.$$

The expansion factors  $c_v$ ,  $q(\rho)$ ,  $d_v$  and  $p(\rho)$  are fined with the help of the orthogonality relations.





If the scattering happens on statistic irregularities, the averaging of the scattered radiation power on an ensemble is applied. Then the full intensity transferable in the waveguide or, for example, the power of the radiation stipulated by the scattering of the directed modes on the irregularities can be found. Thus, the solution of the direct scattering problem can be obtained as the field solution, i.e. as the peak-phase distributions, or as the solution circumscribing distribution of the intensity of the laser radiation scattered on irregularities. These expressions describe both the scattering on the irregularities of the waveguide and on the heterogeneities of the refraction index of the waveguide mediums.

To estimate the radiation losses of waveguide mode power due to waveguide scattering, we should find the full power, transferable by all propagating TE modes of an asymmetric irregular optical waveguide as follows:

$$P_{\Sigma} = P\left\{\sum_{\nu} |C(\nu,\beta)|^{2} + \sum_{1}^{2} \int_{0}^{+\infty} |q(\beta,\beta_{\nu})|^{2} d\rho\right\}.$$
 (7)

Our computer modeling according equation (7) demonstrates e.g. that in an integrated-optical waveguide with the surface roughness geometrical parameters  $\bar{\sigma} = 4.2$  nm (surface roughness rms high) and  $\bar{r} = 0.18$  µm (surface roughness correlation interval) the losses of the guided mode can achieve 6-10 dB/cm.

One can achieve some decrease of radiation losses in this case by means of the certain optimization of parameters of the waveguide under consideration, for example, by chosen of an optimal value of the longitudinal component of the propagating constant  $\beta_0 = k\gamma$  of the guiding mode [39] ( $\gamma$  is the effective refraction index of the waveguide or an effective coefficient of waveguide phase slowing). We can define needing  $\gamma$  via resolving the dispersion relation for investigating waveguide (see the next paragraph of this paper).

# 3. Dispersion relations and results of numerical calculations for three layer regular waveguide

For simulation the well known representation of dispersion relation in a trigonometrical kind for thee layer waveguide was used:

$$\rho_f h = \operatorname{arctg}(\rho_c/\rho_f) + \operatorname{arctg}(\rho_s/\rho_f) + (m-1)\pi,$$

where  $\rho_f = k_0 \sqrt{n_2^2 - \gamma^2}$  is the vertical component (for -h < x < 0) of the propagation constant of a directed TE-mode along an axes *z*; *h* is the thickness of a waveguide layer;  $\gamma$  is the factor of phase slowing down (effective waveguide refraction index);  $\rho_c = k_0 \sqrt{\gamma^2 - n_1^2}$  is the vertical component of the propagation constant of a directed TE-mode for x > 0;  $\rho_s = k_0 \sqrt{\gamma^2 - n_3^2}$  is the vertical component of the propagation constant of a directed TE-mode for x < -h; m = 0, 1, 2, ... The dispersing relations  $\gamma = \gamma(h)$  for the first five TE and TM modes of a regular three-layer polystyrene integrated-optical waveguide are represented in the fig. 3.



**Fig. 3**. Dispersing relation  $\gamma = \gamma(h)$  for three-layer polystyrene integrated-optical waveguide.

# 4. Optical nanofibers with random rough surface. Radiation losses in optical nanofibers with random rough surface

In recently published paper [46], the radiation losses in nanofibers are estimated in assumption of sinusoidally perturbed surface. It is demonstrated that for realistic perturbation amplitude, the typical values of the loss coefficient are about  $1-10^{-3}$ dB/mm and substantially depend on the perturbation period and refractive index contrast. Besides, the paper contains the conclusion that the model of sinusoidal perturbation can be generalized for all kinds of the surface deformation by means of Fourier analysis. This statement is controversial because direct generalization of the represented model assumes linear relationship between the amplitude of perturbation and the power of light scattered by this perturbation.

Meanwhile, the radiated power is expressed as the square of linear functional of perturbation amplitude and thus can not be represented as a sum of independent contributions of perturbation's Fourier components. This problem is solved with a help of statistical approach, when the perturbed surface is treated as a random field and the radiated power is determined with averaging over perturbation ensemble.

The statistical approach to the problem of light scattering in randomly perturbed waveguides, first developed in early studies of Marcuse [14, 48], was used in [41, 42] in order to estimate the lower bound of intrinsic losses in photonic crystal fibers. The mean radiated power is expressed through the power spectral density of the random roughness and this relation has the linear character. Marcuse's approximation is quite good for weakly guiding fibers but it sets aside the following.

It is well known [49] that the solution of Maxwell equations for inhomogeneous medium in the first approximation of the small perturbation method has a form of linear relation between the mean power of the scattered wave and the power spectral density of refractive index fluctuations. It is demonstrated [48] that the perturbation of the waveguide surface can be represented with equivalent perturbation of the refractive index. The refractive index perturbation is expressed as discontinuous function of the amplitude of the surface roughness. As this relation can not be linearized, the radiated power must have nonlinear form of dependence on the roughness power spectrum even in the first approximation of the small perturbation method. This means that a part of the scattered power, proportional to low frequency components of the roughness spectrum, is lost in the linear solutions. As the power spectrum has inverse-square law of dependence on the spatial frequency [43], the scattering on harmonics of the small frequencies can be considerable.

It was established former [50] that the power spectrum of refractive index fluctuations in perturbed planar waveguide can be expressed through the roughness correlation with a help of Price's theorem about nonlinear operations over Gaussian random field [51, 52]. In the present paper, we establish the relation between the radiation losses and the power spectrum of the rough surface of nanofiber, and to estimate the loss value.

Following [6, 40, 46], the rough surface of a fiber waveguide (fig. 4) is represented as a variation of its radius  $\rho$ :

$$\rho(z,\varphi) = \rho_0 + \xi(z,\varphi). \tag{8}$$

In equation (8)  $\rho_0$  is the radius of unperturbed waveguide, the function  $\xi(z, \varphi)$  describes the perturbation (see fig. 4).

We take that  $\xi$  is the uniform Gaussian random field [12] with zero mean and statistical correlation function, which depends on the residual coordinates  $\Delta_z = z_2 - z_1$ ,  $\Delta_{\varphi} = \varphi_2 - \varphi_1$ :

$$\left\langle \boldsymbol{\xi}^{*}(z_{1},\boldsymbol{\varphi}_{1})\boldsymbol{\xi}(z_{2},\boldsymbol{\varphi}_{2})\right\rangle = \boldsymbol{\sigma}_{\boldsymbol{\xi}}^{2}\boldsymbol{\gamma}_{\boldsymbol{\xi}}(\Delta_{z},\Delta_{\boldsymbol{\varphi}}),$$

where  $\sigma_{\xi}^2$  is the roughness variance,  $\gamma_{\xi}$  denotes normalized correlation. We suppose the perturbation magnitude  $\xi$  being small. The small order of  $\xi$  means that the amplitude of electric field of both propagating and radiation modes can be considered constant within the perturbed region. As in nanofibers the perturbation is less in scale than 1 nm [44], the small order condition holds with high accuracy.

We confine the consideration to the most important case of single-mode operation of the waveguide. So, the propagating light wave has the appearance of the fundamental HE<sub>11</sub> mode with electric component  $\mathbf{E}_{11} = \mathbf{e}_1(r, \varphi) \exp(i\beta_1 z)$ .

The scattered wave is expressed as a superposition of radiation ITE and ITM modes:

$$\mathbf{E}_{v}^{r} = \mathbf{e}_{v}^{r}(Q; r, \boldsymbol{\varphi}) \exp(\pm i\boldsymbol{\beta}(Q)z),$$

where  $Q^2 = \rho_0^2 (k^2 n_{cl}^2 - \beta^2)$ , the signs "+/-"correspond to the forward and backward propagating modes, respectively, and:

$$\mathbf{e}_{1}(r,\varphi) = \mathbf{\Psi}_{1}(r) \exp(i\varphi).$$
  
$$\mathbf{e}_{\nu}^{r}(Q;r,\varphi) = \mathbf{\Psi}_{\nu}^{r}(Q;r) \exp(i\nu\varphi), \quad \nu = 0,\pm 1,\pm 2...$$

The total mean power, radiated with the random roughness, is expressed with integral over the whole of system of radiation modes [14, 40, 48].

The loss coefficient is obtained as:

$$\eta = -10 \lg \left( 1 - \frac{P_{\text{rad}}}{\overline{P}} \right) / L \,. \tag{9}$$

In equation (9)  $\overline{P}$  is the power of the fundamental mode; *L* is the length of fiber. It follows from our results that radiation losses are linear in *L*.

We applied the proposed theoretical model to estimate the radiation losses caused with the rough glass/air interface of the nanofibers. The physical parameters of the model were chosen so as to make possible comparison with the reported experiments [44, 45]. For the lack of data, we confined the calculation to the case of the silica fiber, for which we accepted  $n_{co} = 1.46$ .



**Fig. 4.** Perturbed fiber waveguide.  $n_{co}$ ,  $n_{cl}$ , are the refractive indices of the core and the cladding (air), respectively.

The dependence of the loss coefficient on the fiber diameter was calculated for the wavelength  $\lambda = 633$  nm (see fig. 5).

We should note that the perturbation power spectrum is expected to have inverse-square low, therefore, the contribution of the low frequencies is very critical, and could be explained in terms of the effective depth of the perturbed layer.

Note that passage to the limit of spatial frequencies  $\beta_{cut} \rightarrow 0$  gives the reasonable estimation of losses, but leads to the growth of the effective depth of the perturbation to the values which exceed the waveguide diameter. To our opinion, the extremely low frequency perturbations with large amplitudes should be understood as random waveguide bends. Naturally, there are no reasons to describe such perturbations with the inverse-square law spectrum. So, the estimation of radiation losses in the silica nanofibers with D < 180 nm has rather qualitative character.



Fig. 5. Dependence of the loss coefficient on the fiber diameter, in dB/mm. a) Linear approximation (dash), nonlinear loss component (dot), aggregate losses (solid),  $\beta_{cut} = 0$ . b) Losses for different cutoff frequencies of surface perturbation,  $\beta_{cut} = 1.0 \text{ mm}^{-1}$  (blue),  $\beta_{cut} = 0.1 \text{ mm}^{-1}$  (red),  $\beta_{cut} = 0$  (black).

The calculated losses are somewhat less in value than those observed experimentally. Apparently, the suggested model is approximate, and sets aside some important particularities of the experiment. With it, the model must be useful in understanding of losses in optical nanofibers, caused with intrinsic roughness of glass/air interface.

### 5. Conclusion

All facts following from the presented paper should be taken into consideration, when one needs to synthesize e.g. an optical processor or/and optical sensor with high metrological parameters [4, 7, 9, 12, 13, 37-40, 44, 53-58].

In summary we should noted that the offered methods can be applicable for analysis of similar dielectric, magnetic, optic and meta materials structures in enough broad band of electromagnetic wavelengths.

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